



Associação Brasileira de Mecânica dos Solos e Engenharia Geotécnica

*Aprendendo com o passado,
celebrando o presente e
inspirando o futuro*

21 e 22 de julho de 2025
Centro de Convenções Rebouças
São Paulo, SP

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Collapsible soils in Argentina

Experiences and case histories

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Former VP-ISSMGE

Former President SAIG

Former Dean UNC

SAIG – UNC



LOESSIAL SOILS

Loess Definition & General Description (after Rinaldi 2009)

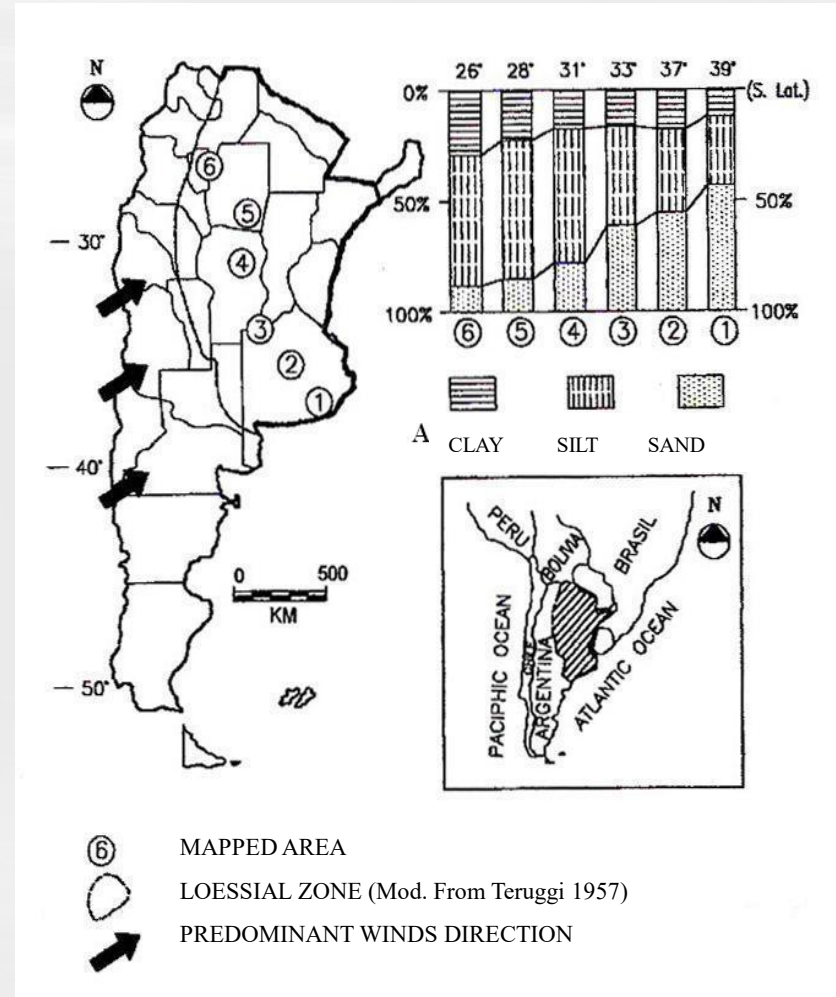
- German Term: Loose
- Wind-Blow Formation
- Platy Silt and Sand Particles (oriented in the depositional direction).
- Minor clay fraction (illite and montmorillonite).
- Double Porosity (macro and micropores)
- Water soluble and non-soluble salts
- Unsaturated in natural state

Distribution In The World (after Rinaldi 2009)



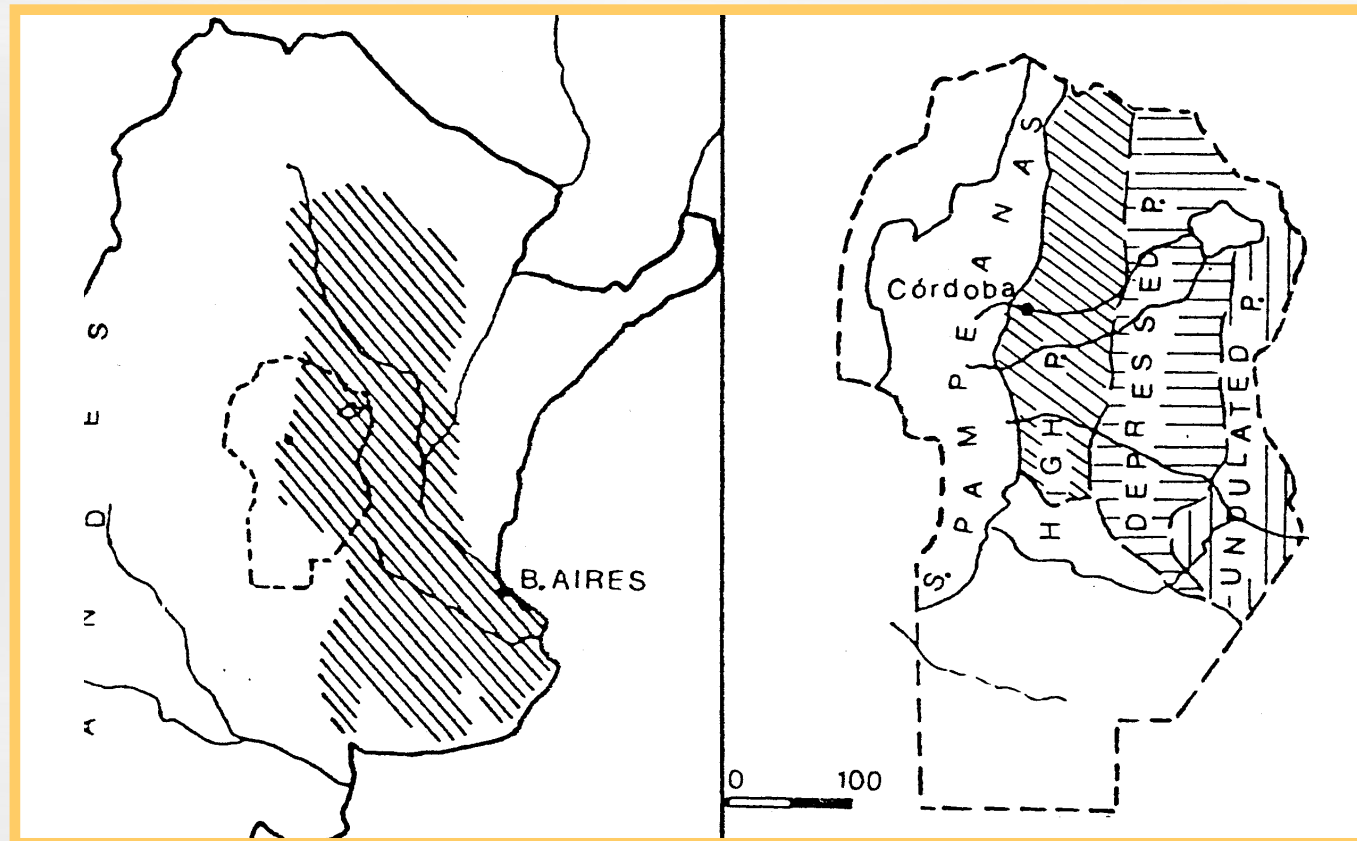
- 10 % of the total continental surface: 13.000.000 km²
- Thickness: Few meters up to 300 m
- West Valley Mississippi River and East of Washington
- Largest Deposits:
North Hemisphere: China

Argentinian Loess Origin (after Rocca et al. 2006)



Distribution In Argentina

(After Rocca et al 2006)



Main Properties (after Rinaldi 2009)

- Color: Brownish to yellow
- Very stable at low water content
- High volume change when loading or wetting (collapse)
- Higher vertical permeability
- High susceptibility to surface erosion and piping

Average properties of ancient pampean loess

The elevations refer to the level of the Paraná River.

Zone	Deep (m)	Elev. (m)	e_o	ω (%)	ω_L (%)	ω_p (%)	IP (%)	Cc	$\underline{C_sCr}$	γ_s (kN/m ³)	γ
Ia)	10.16	15.00	0.848	32.0	67.0	30.0	37.0	0.32	0.024	25.98	18.53
Ia)	12.16	13.00	0.888	33.5	67.0	31.5	35.5	0.33	0.025	25.98	18.33
Ib)	20.00	5.16	0.826	31.4	41.3	27.8	13.5	0.15	0.010	25.78	18.53
Ib)	27.20	-2.04	0.848	32.0	51.0	30.0	21.0	0.18	0.012	25.98	18.53
Ic)	32.70	-7.54	1.180	44.5	69.0	33.5	35.5	0.28	0.020	25.98	17.25

Properties of recent loess

Averages and Standard Deviation (STD) calculated in analysis of 420 profiles.

	ω (%)	ω_L (%)	IP (%)	PT4 (%)	PT10 (%)	PT40 (%)	PT200 (%)	γ_d KN/m ³
CL 2A								
AVERAGE	16.08 5.15	24.25 2.84	4.58 1.93	99.93 0.50	99.49 1.81	96.98 4.95	90.64 10.53	12.9 1.07
STD								
CL 2Ax								
AVERAGE	17.37 4.74	24.50 3.32	4.84 1.76	99.62 3.11	99.34 1.58	95.48 6.51	87.82 15.22	13.9 5.00
STD								
CL 2B								
AVERAGE	22.07	26.54	6.71	99.79	98.54	93.39	84.17	14.8
STD	7.78	5.34	3.52	1.04	3.13	13.00	15.55	8.33
CL 2C								
AVERAGE	28.66	35.02	10.86	100.00	99.63	96.61	88.55	13.4
STD	11.16	10.40	6.77	0.00	0.86	6.27	9.87	1.17

(After Rocca et al 2006)

Grain Size Distribution

Grain Size	Content %
Sand (> 0.75 mm)	5 - 15
Silt (0.75 - 0.002 mm)	40 - 60
Clay (< 0.002 mm)	12 - 35
CaCO ₃	2 - 10

Mineral Composition

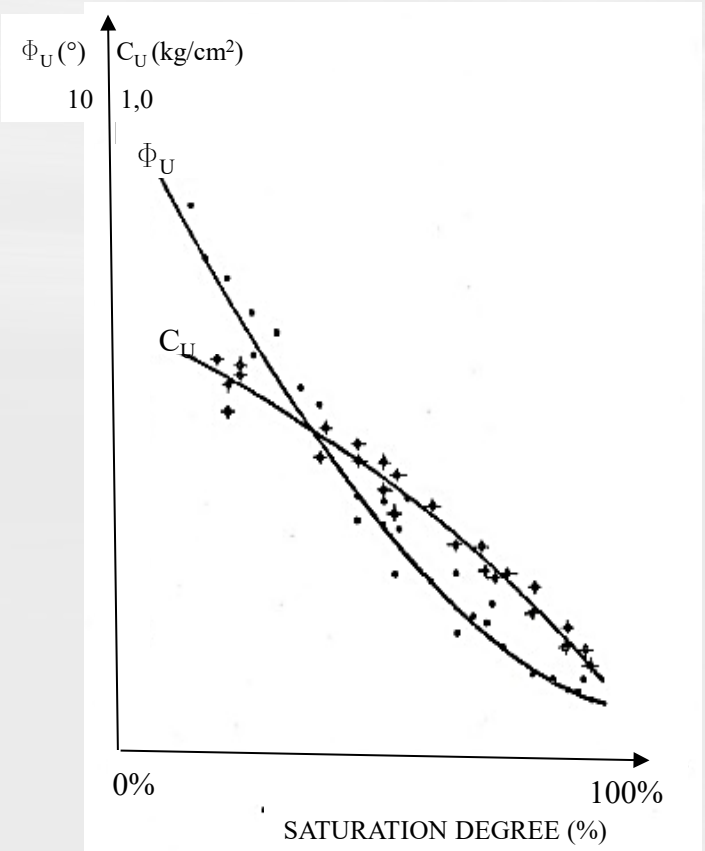
Particle Size	Mineral Components	% Content by weight)
Sand	Quartz (2-30)	20 - 30
	Feldspar (20-65)	20 - 65
	Volcanic Glass (1-25)	1 - 25
	Basalt (1-25)	1 - 25
Silt	Quartz (20-30)	20 - 30
	Feldspar (30)	30
	Volcanic Glass (15-60)	15 - 60
	Gypsum (20)	20
Clay	Illite (90)	90
	Montmorillonite (0-5)	0 - 5
	Kaolinite (0-5)	0 - 5
CO ₃ Ca	Nodules and dispersed	2 - 10

Chemical Composition

Exchangeable Cations (me/100g)					Soluble Cations (me/100g)			
Ca	Mg	Na	K	CEC	Ca	Mg	Na	K
3 - 12	2 - 6	1 - 15	1 - 3	14 - 25	0.1 - 0.5	0.06 - 0.2	0.5 - 4	0.03 - 0.1

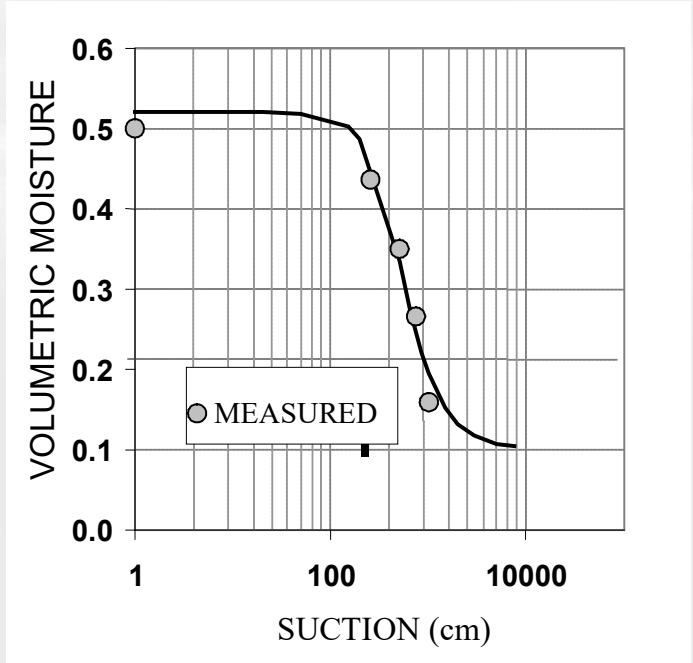
(After Rinaldi 2009)

COLLAPSIBLE LOESSIAN SOILS

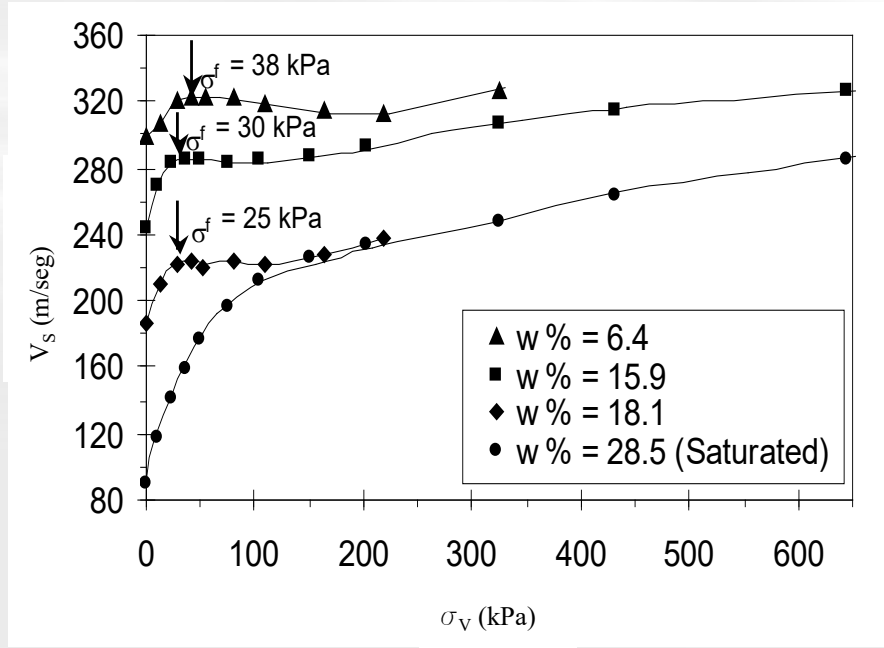


(After Rocca et al 2006)

Main Parameters



(After Terzariol et al 2003)



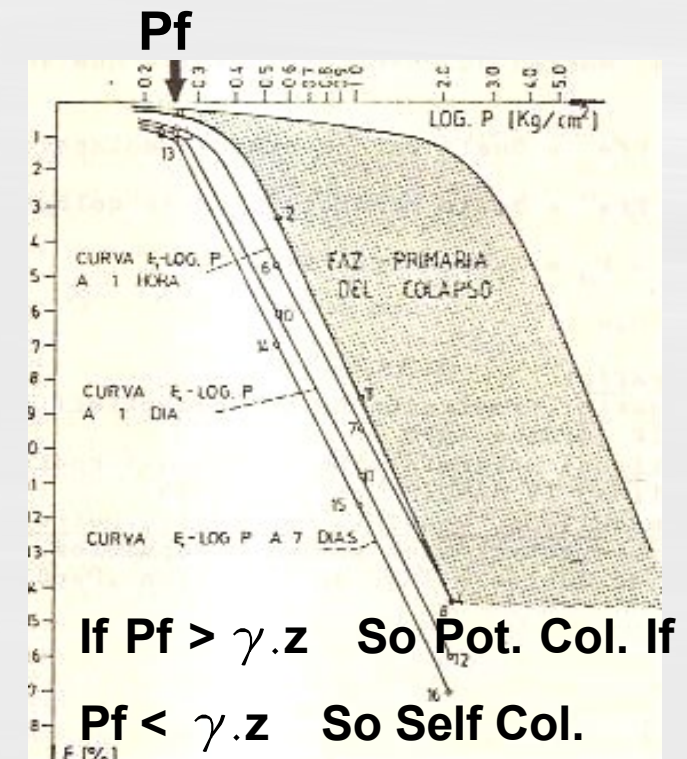
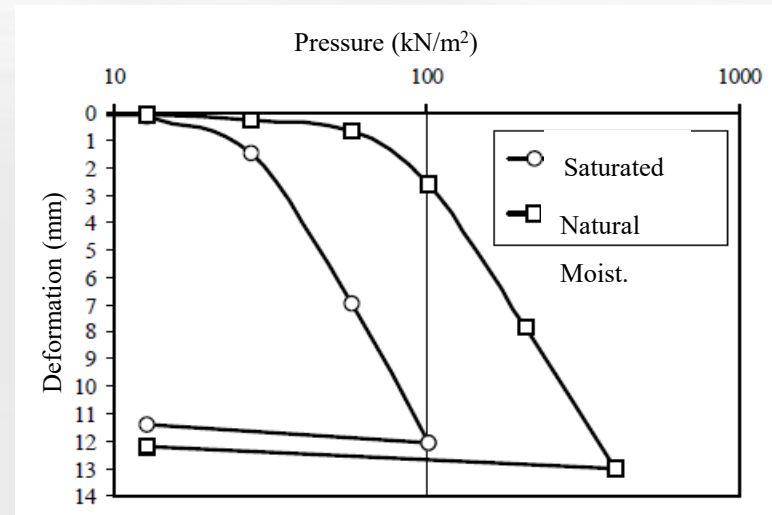
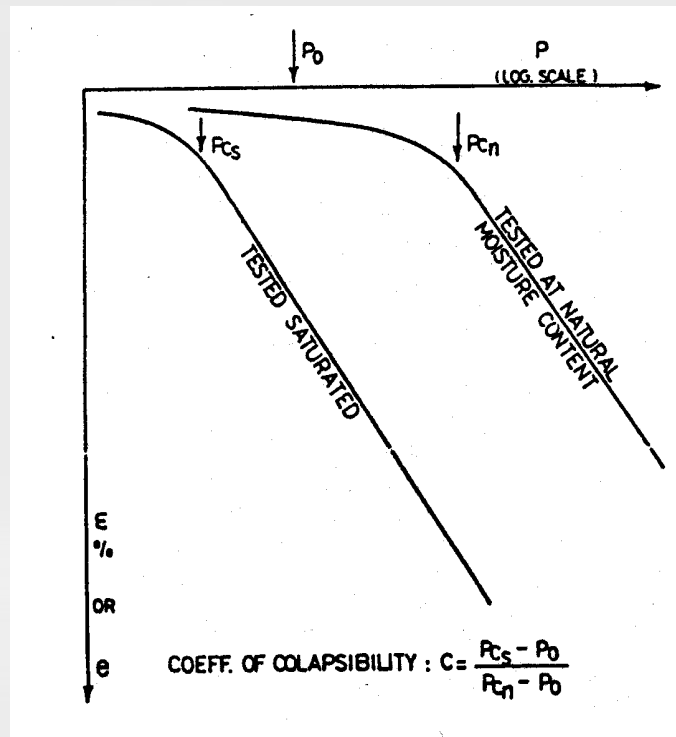
(After Claria 2000)

$$F_s = \frac{\sigma_w}{\sigma_s} = a n^{(p-m)} \theta_v^{-p}$$

(After Francisca et al 2024)

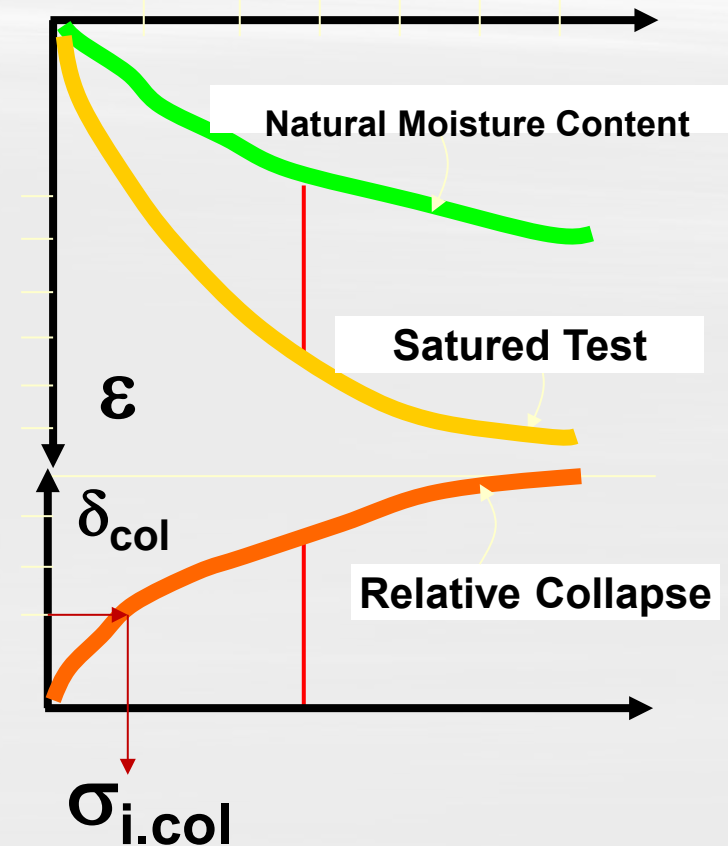
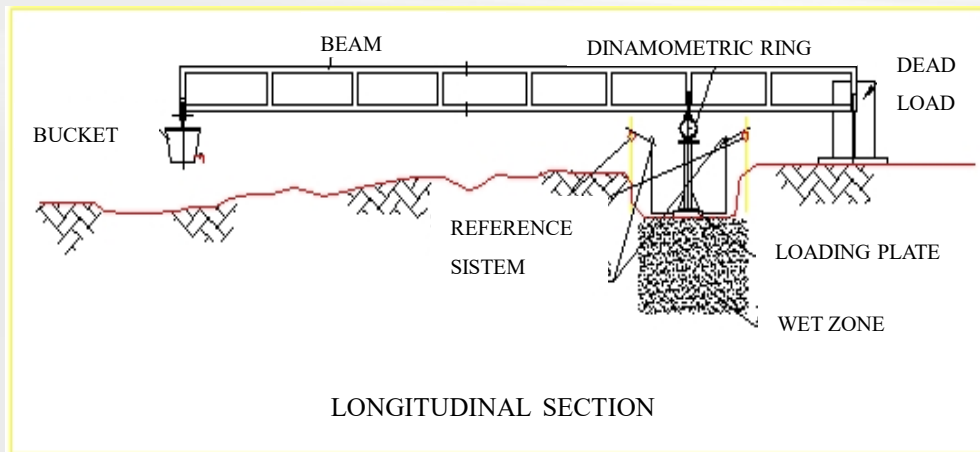
Mechanical Characterization

Laboratory Tests (after Redolfi 1980 – Rocca et al 2006)

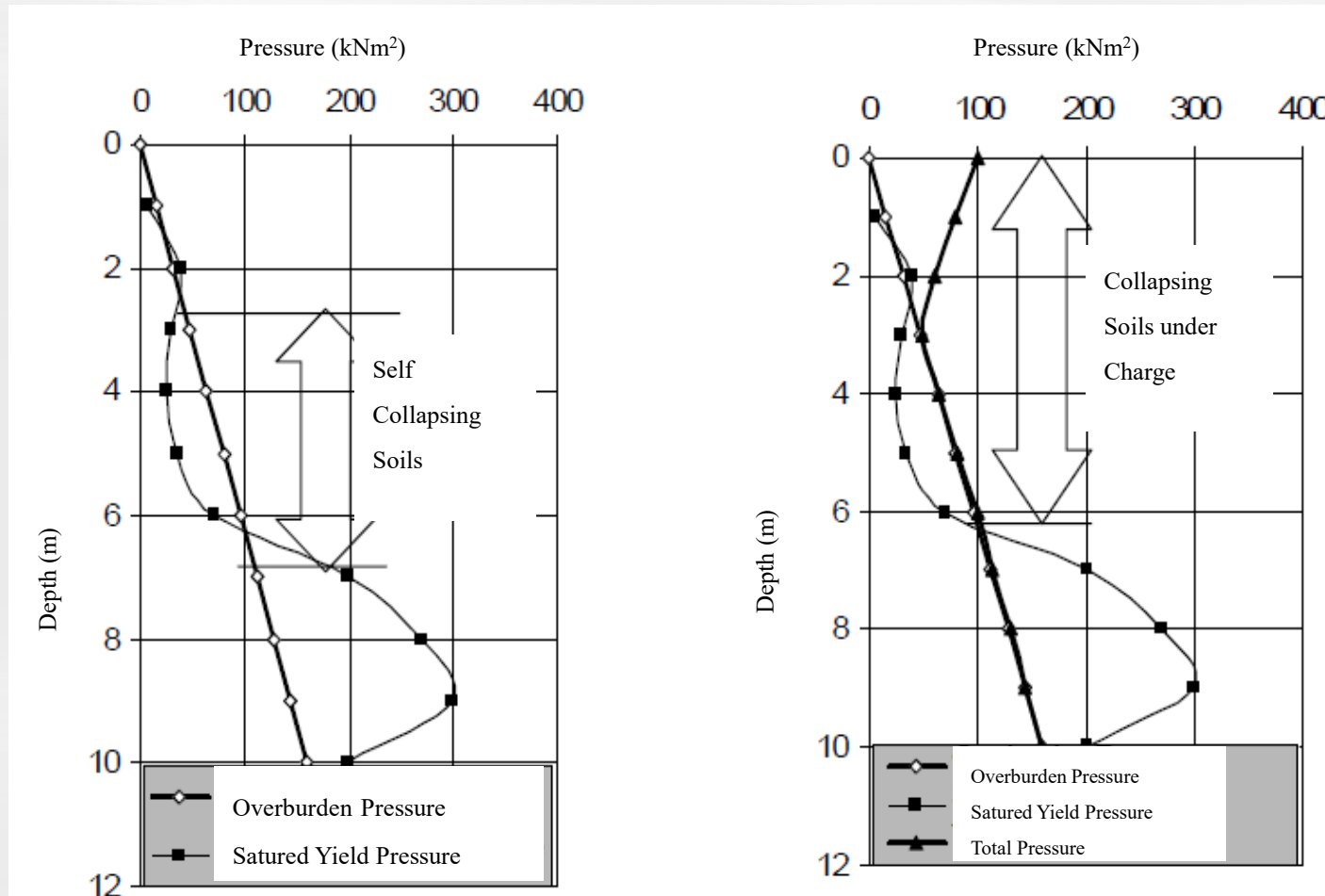


In Situ Tests

(After Terzariol et al 1999)



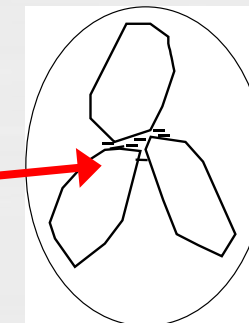
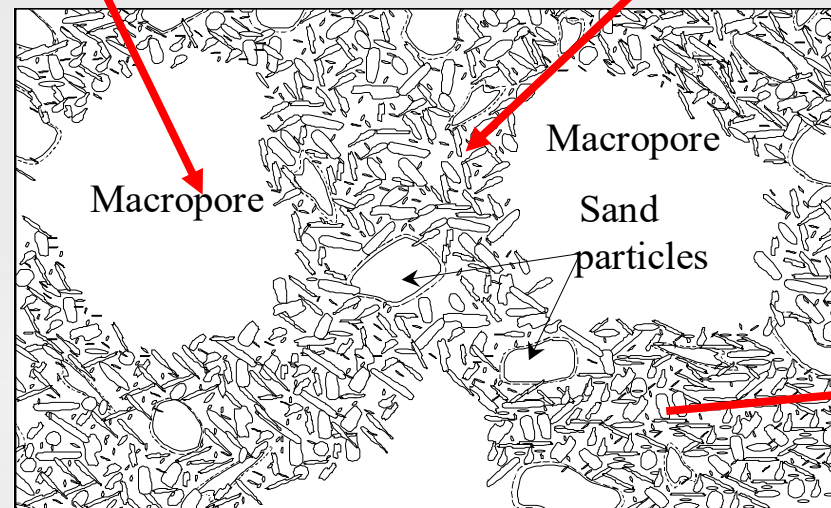
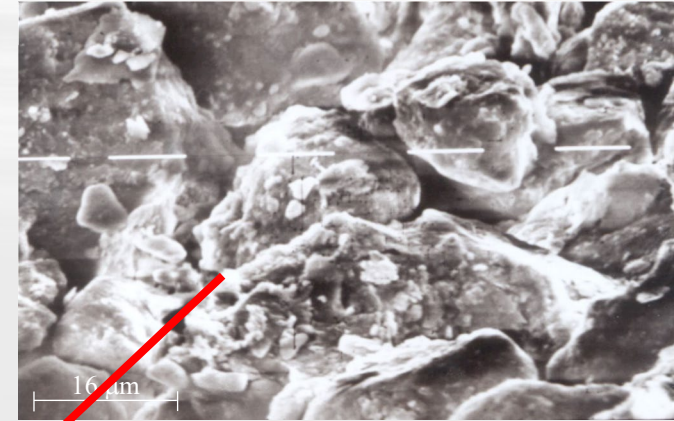
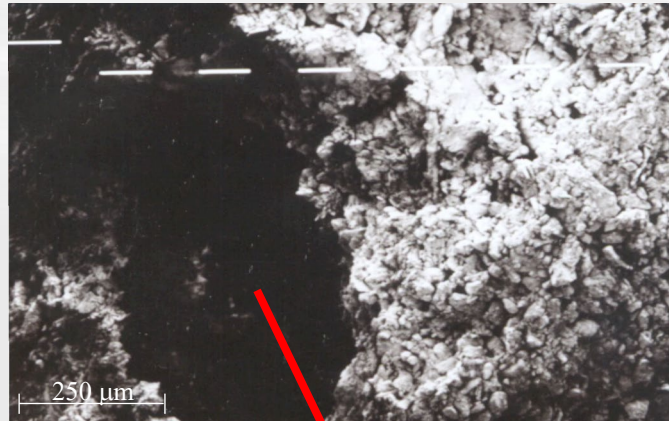
Collapseability Profiles (after Rocca et al 2006)



Comparison between collapse and consolidation processes

PROPERTY	COLLAPSE	CONSOLIDATION
Initial Saturation Degree	Non Saturated	Saturated
Void Ratio	High	High
Water Flux during process	Absorption	Expulsion
Pore Pressure	Tend to Dissipate	Increase Quickly
Process duration in Lab	10 or 20 minutes	Days/Weeks
Shear Strength Before	High	Low
Shear Strength After	Low	High

INTERNAL STRUCTURE OF LOESS



Mechanism of Soil Collapse

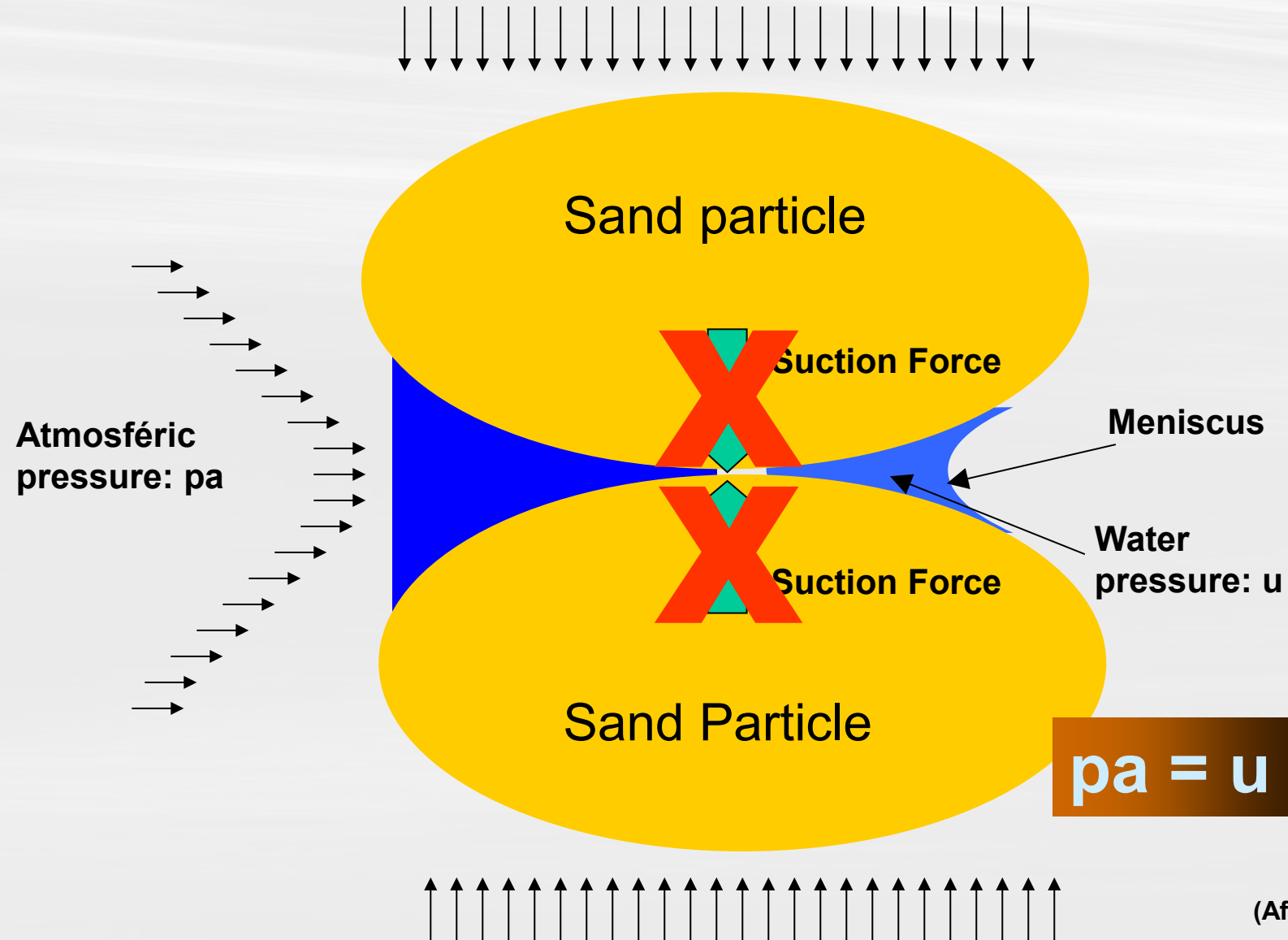
- Weakens of Inter-particle Bonds
- Shear Stresses Concentration and Failure
- Particle Sliding and Closure of Pores

Reduction of
Suction Forces

Dissolution
of Salts

Collapsible soils in Argentina

Experiences and case histories



(After Redolfi 2007)

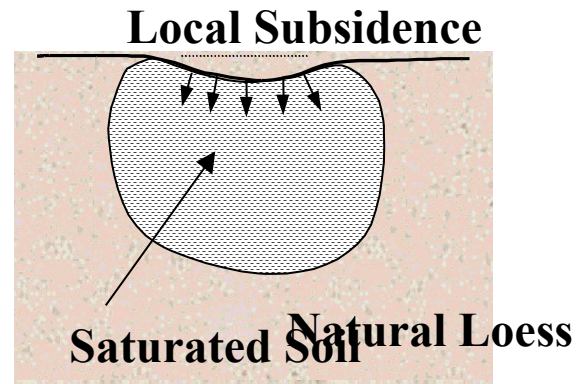
Slaking Test

Before Starting

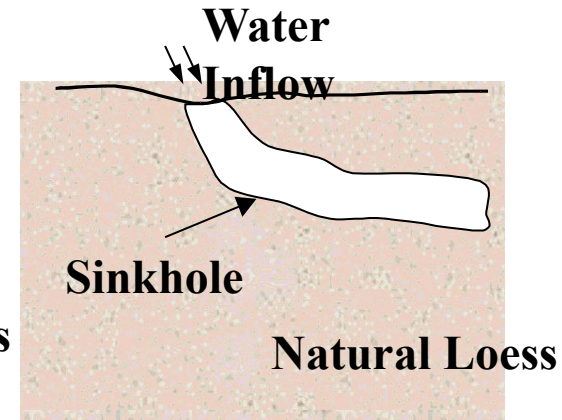


ENGINEERING PROBLEMS IN COLLAPSIBLE SOILS

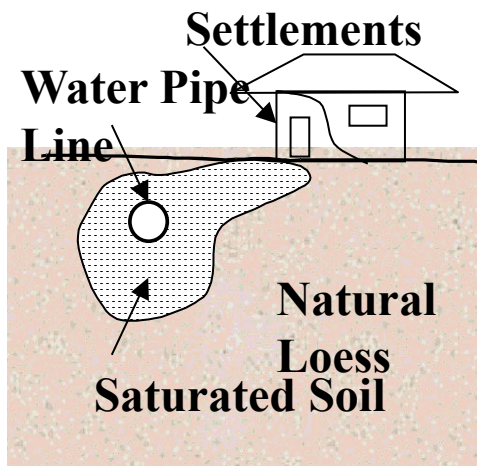
Effects of Water



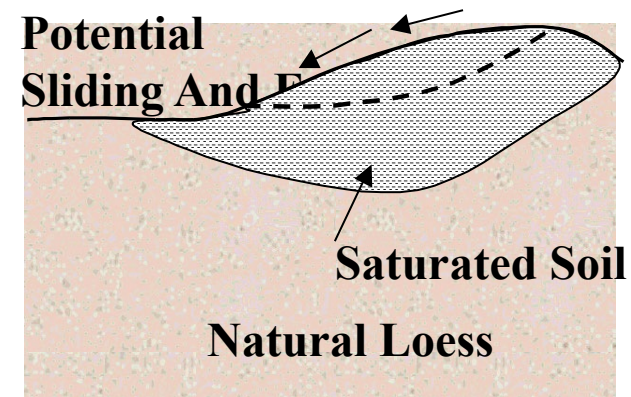
(a)



(b)



(c)



(d)

(After Rinaldi 2006)

Collapsible soils in Argentina

Experiences and case histories

Effects on Foundtions



(After Terzariol 2012)

Erosion



(After Terzariol 2012)

Collapsible soils in Argentina

Experiences and case histories

Piping



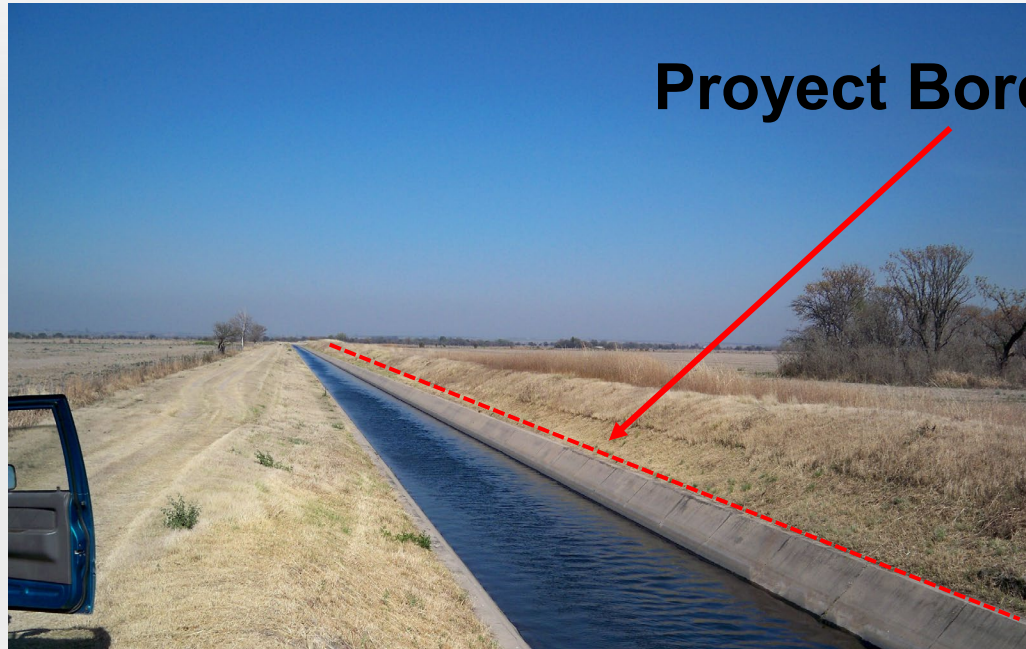
(After Terzariol 2007)

Buried Pipelines



(After Terzariol 2007)

Local and General Subsidence



(After Terzariol 2012)

Sliding on urban excavations (After Terzariol 2025)



ENGINEERING SOLUTIONS

**IMPROVE
SOIL**

**PREVENT SOIL
WETTING**

**MITIGATE
EFFECTS**

**DEEP
FOUNDATIONS**

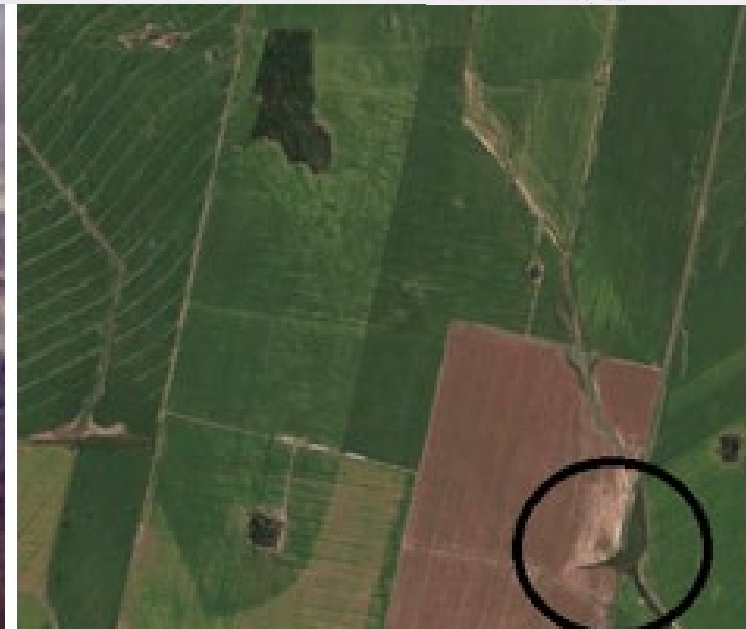
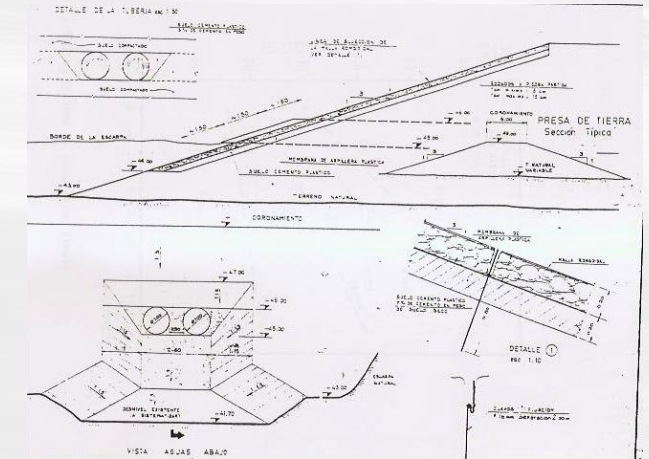
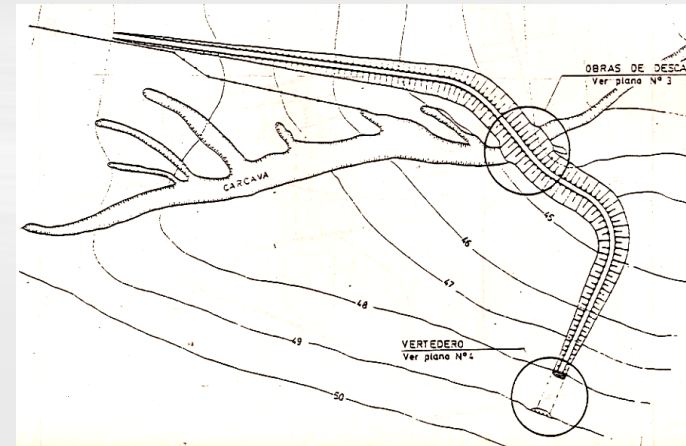
PREVENT SOIL WETTING



(After Terzariol 2006)

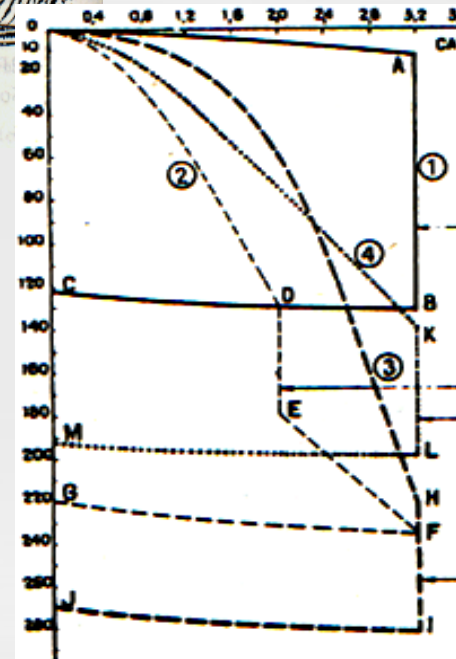
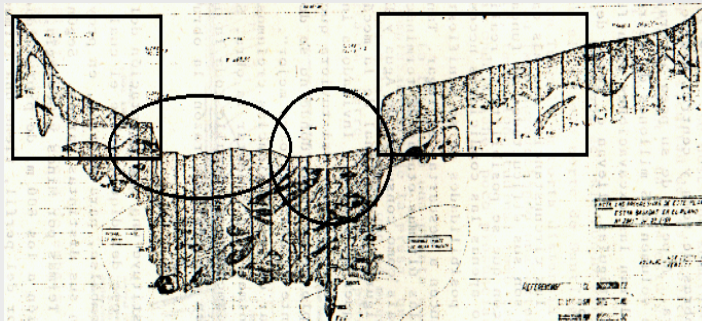
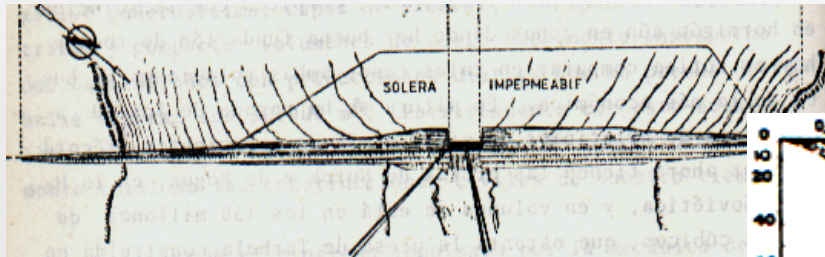
EROSION CONTROL

(After Abbona et al 1989)



DAMS

Foundations Pre Wetting



Use Loess Soil as Construction Material

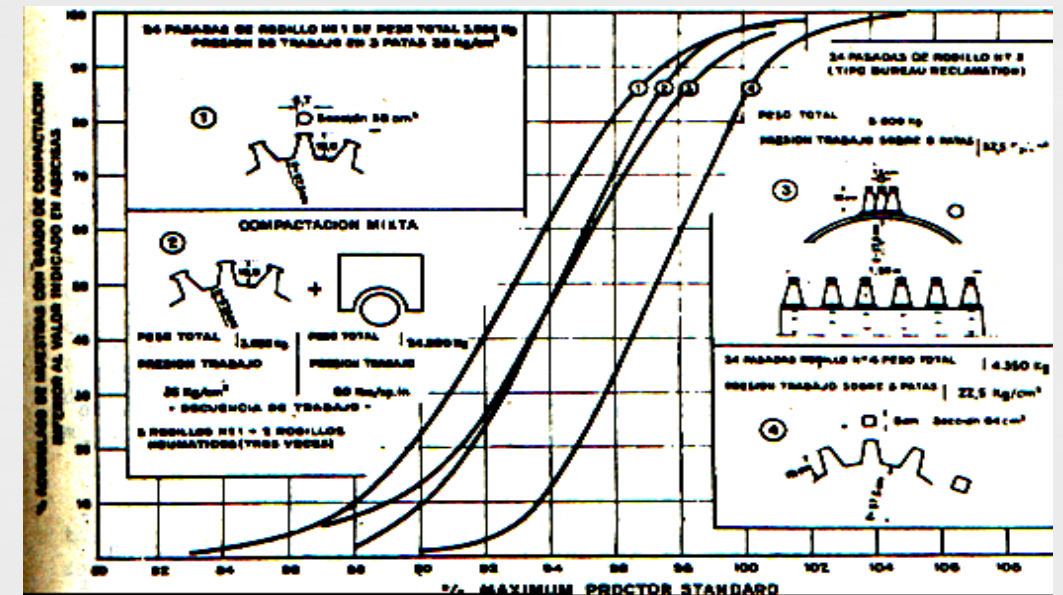
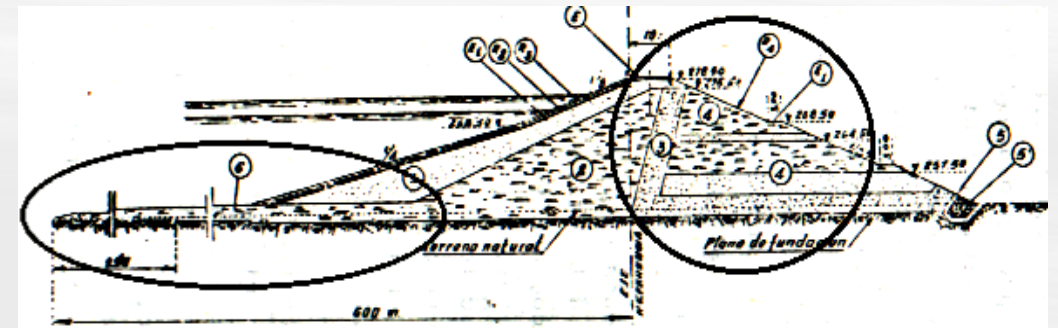
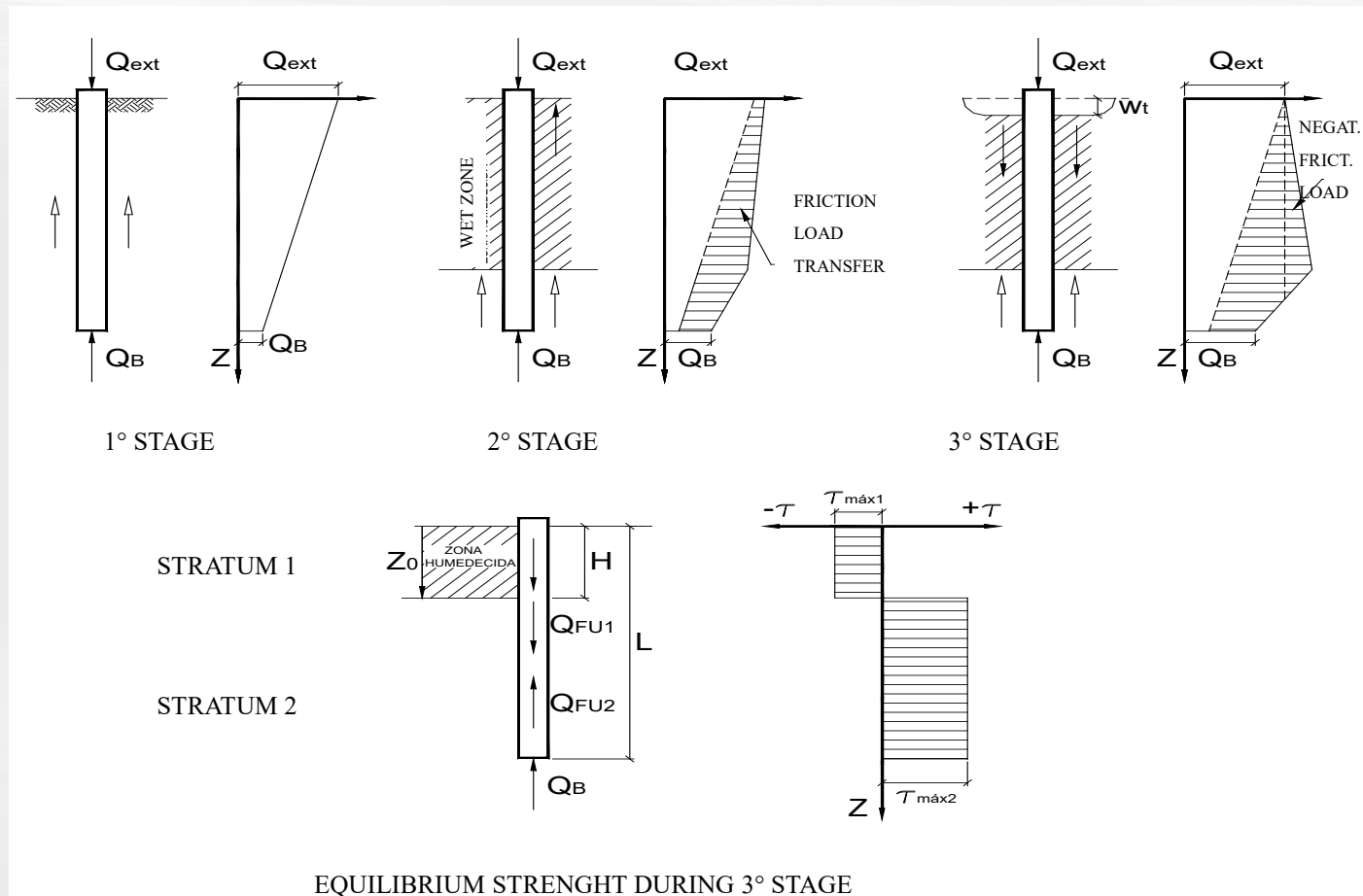


Diagrama de corte transversal de un canal de concreto armado con revestimiento impermeable y geotextil. El canal tiene una anchura superior de 4.00 m y una anchura inferior de 5.00 m. La altura del canal es de 2.50 m. El canal está revestido con una membrana impermeable y una membrana Geotextil. El canal está construido con bloques de hormigón confinados en paneles celulares y vinculados por tendones. El canal está rodeado por una zanja de guarda y una escorrentía. El canal está construido sobre una base de suelo cemento plástico elaborado.

DEEP FOUNDATIONS

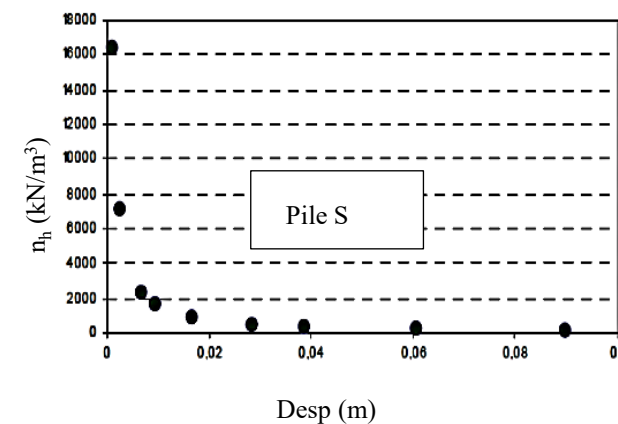
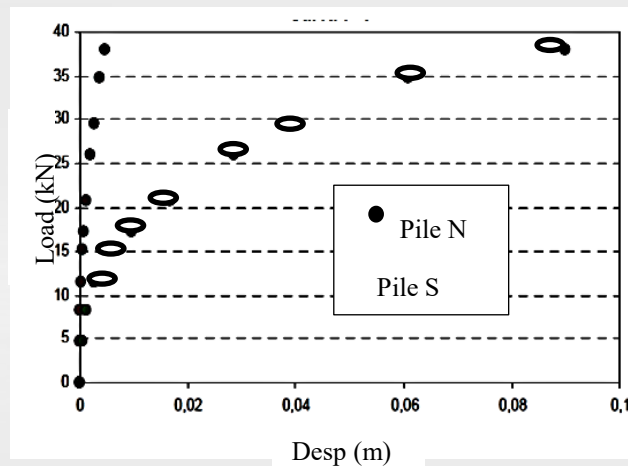
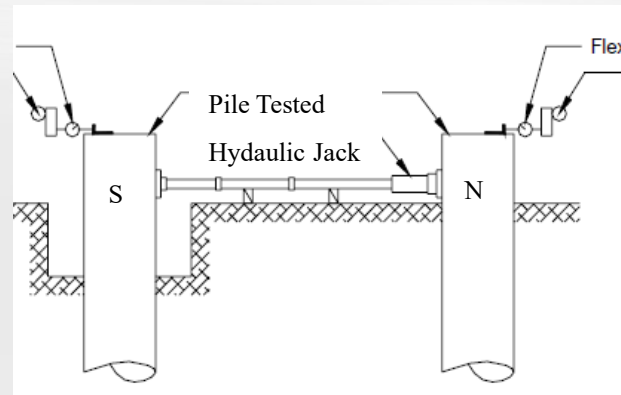
Vertical Loads (After Redolfi et al 1992)



DEEP FOUNDATIONS

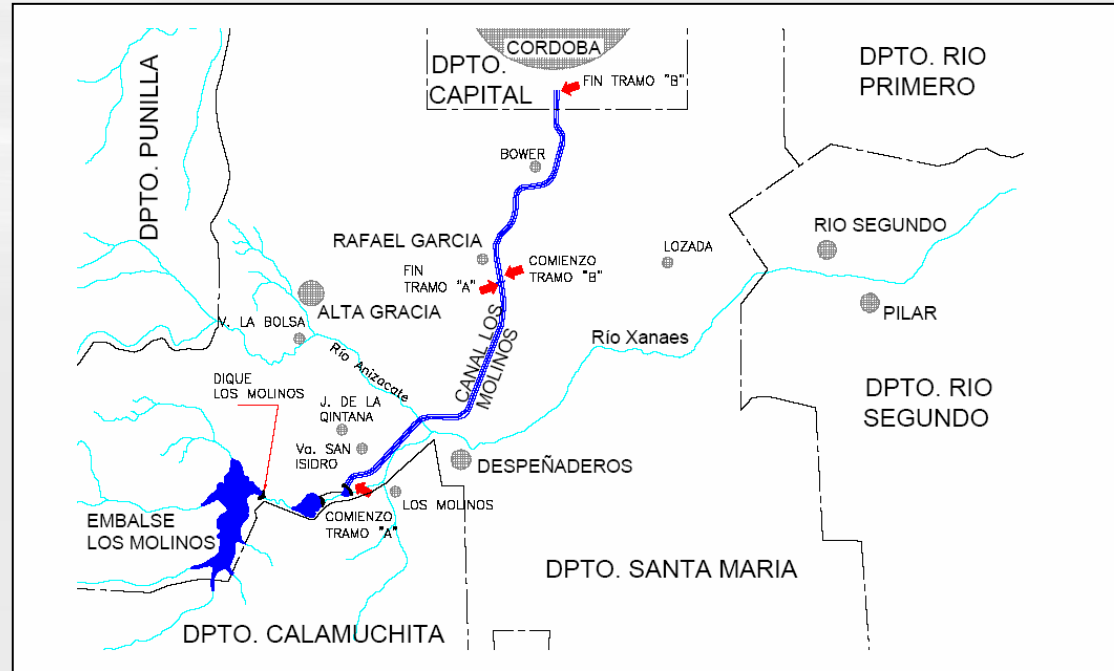
Lateral Loads

(After Terzariol 2006)

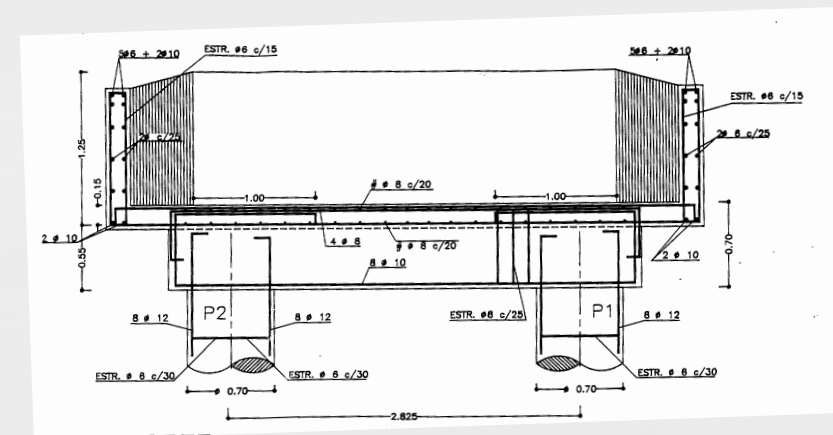
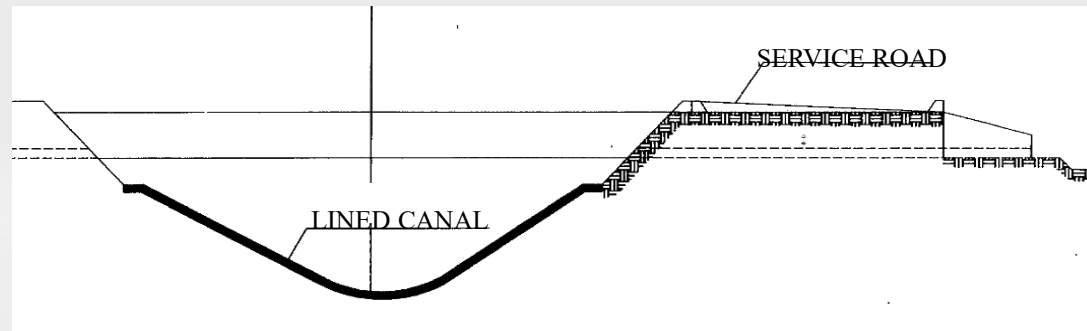


HISTORY CASES

“Los Molinos-Córdoba” Canal



(After Terzariol 2012)



Collapsible soils in Argentina

Experiences and case histories

(After Terzariol 2012)

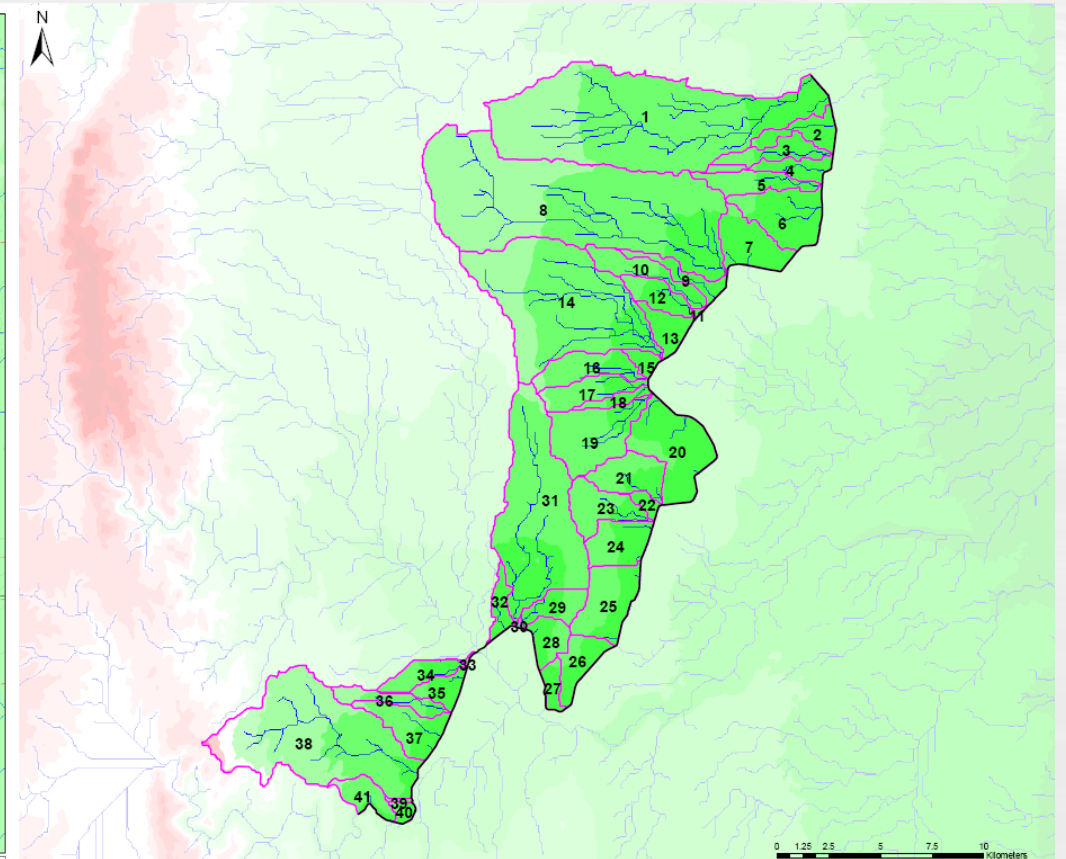
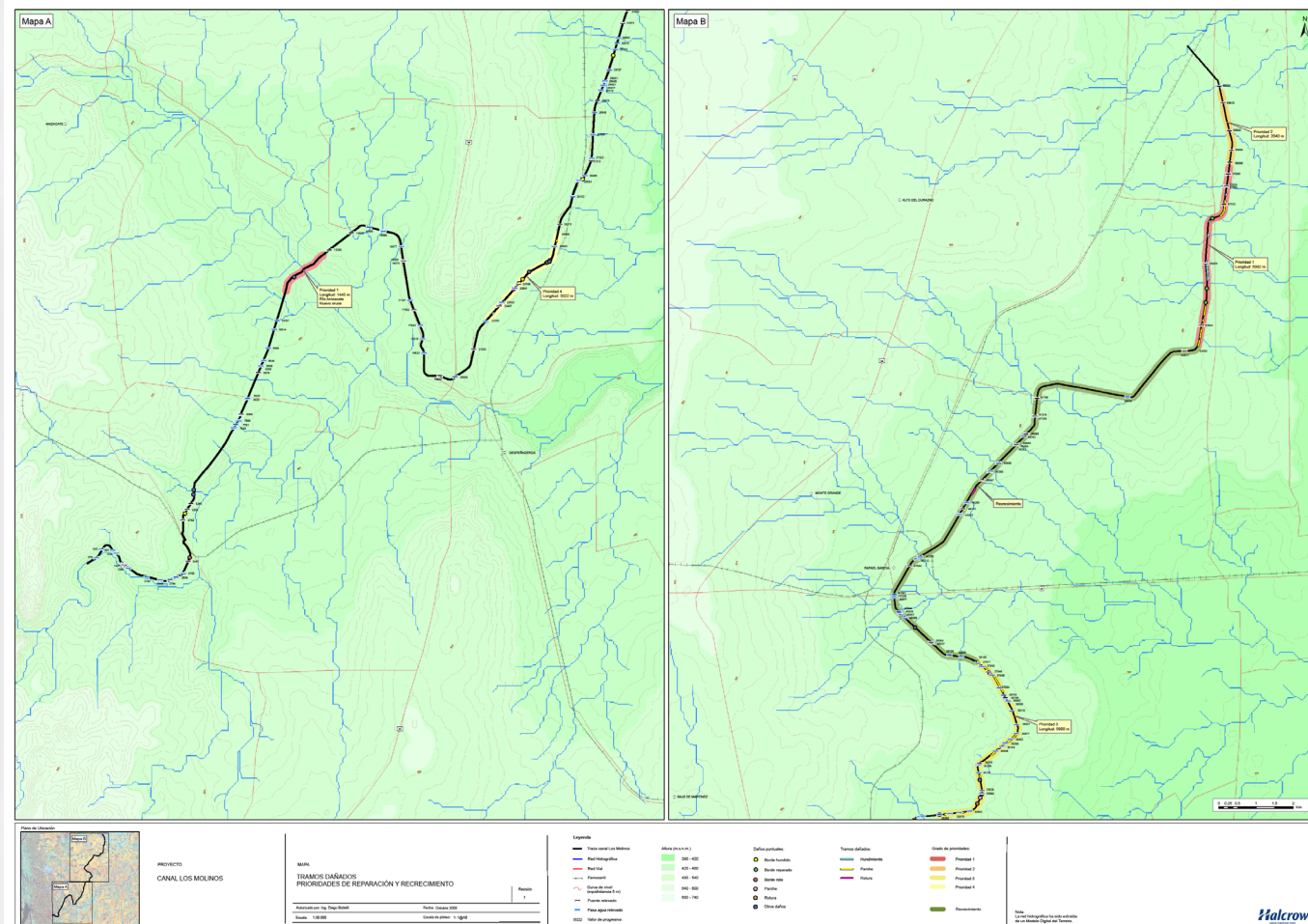


Collapsible soils in Argentina

Experiences and case histories



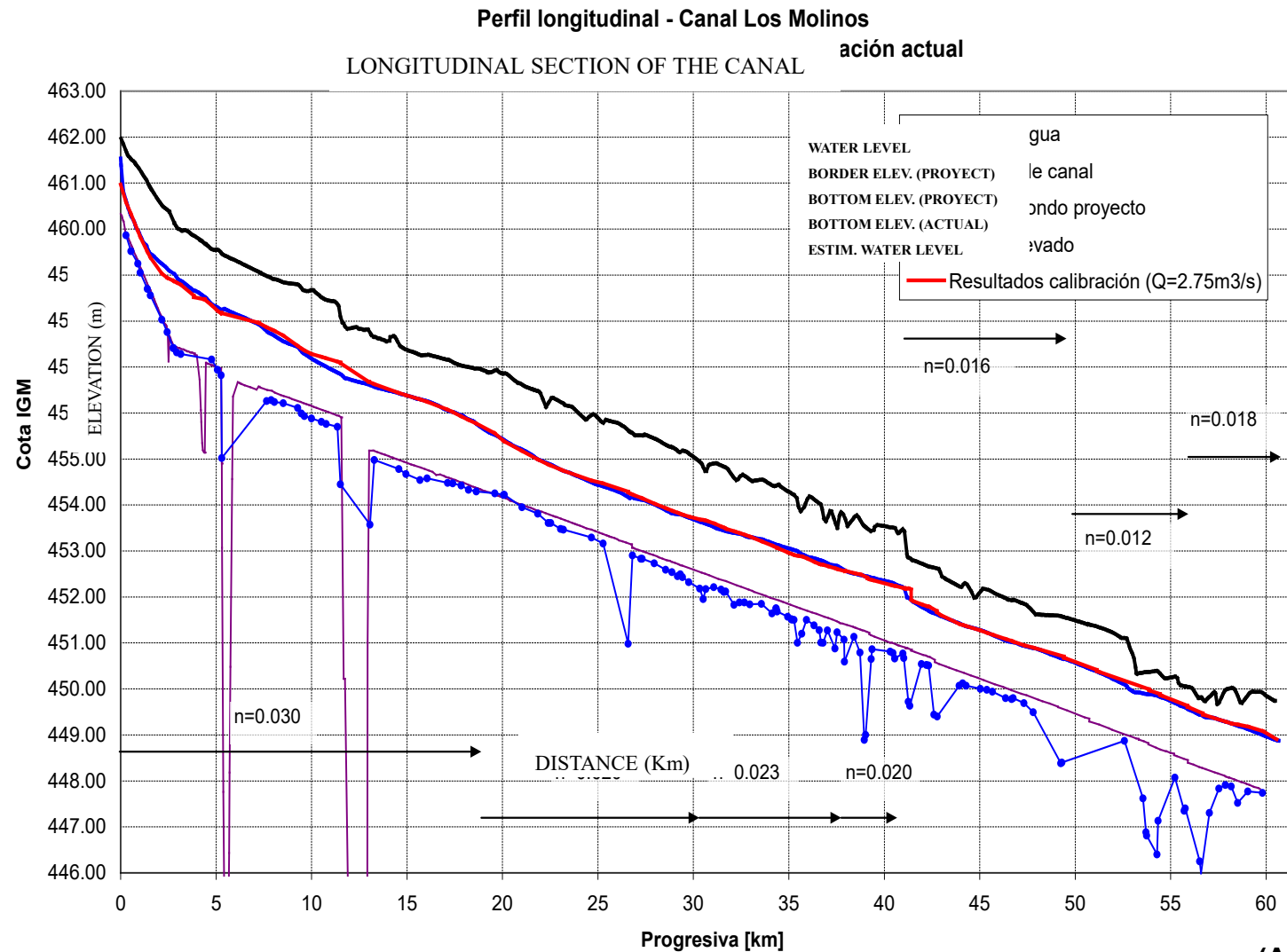
(After Terzariol 2012)



(After Terzariol 2012)

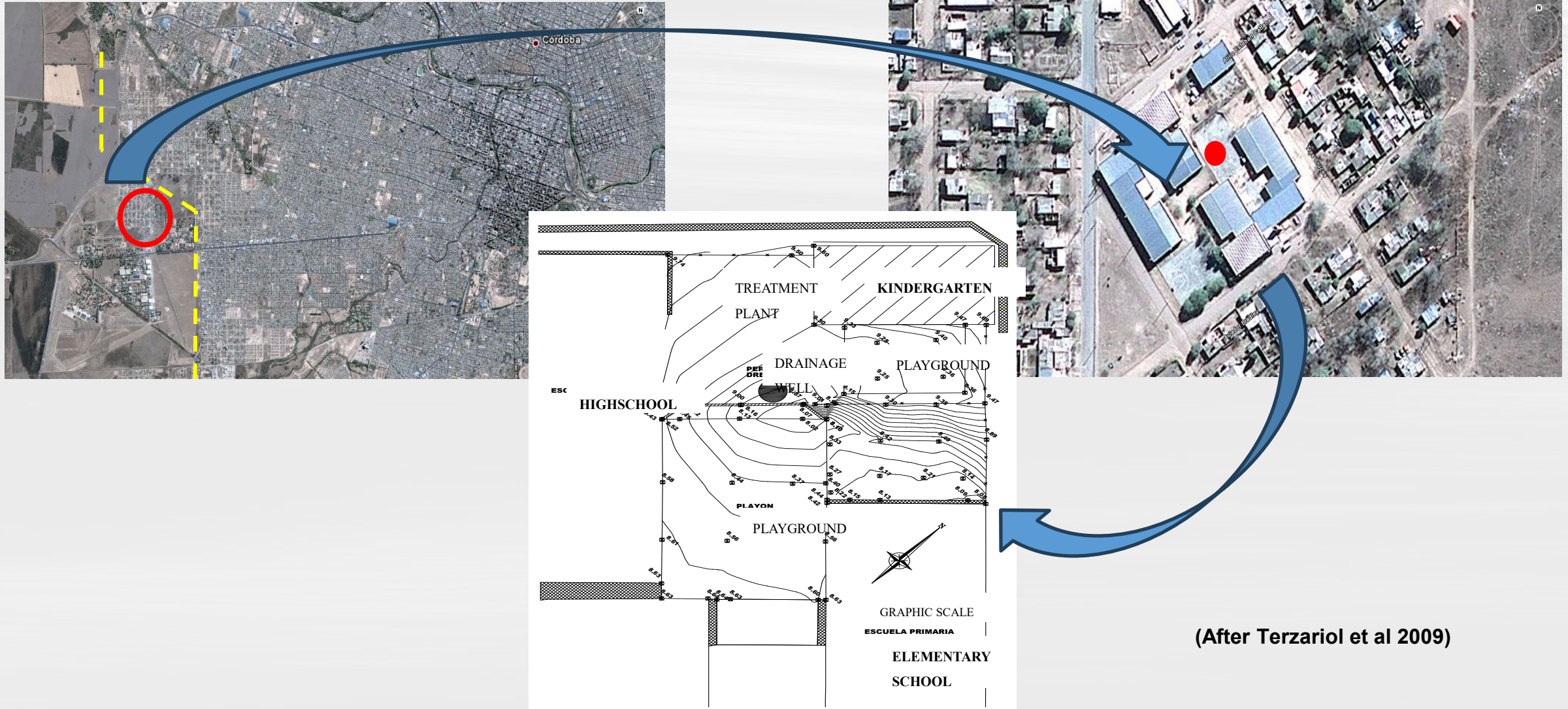
Collapsible soils in Argentina

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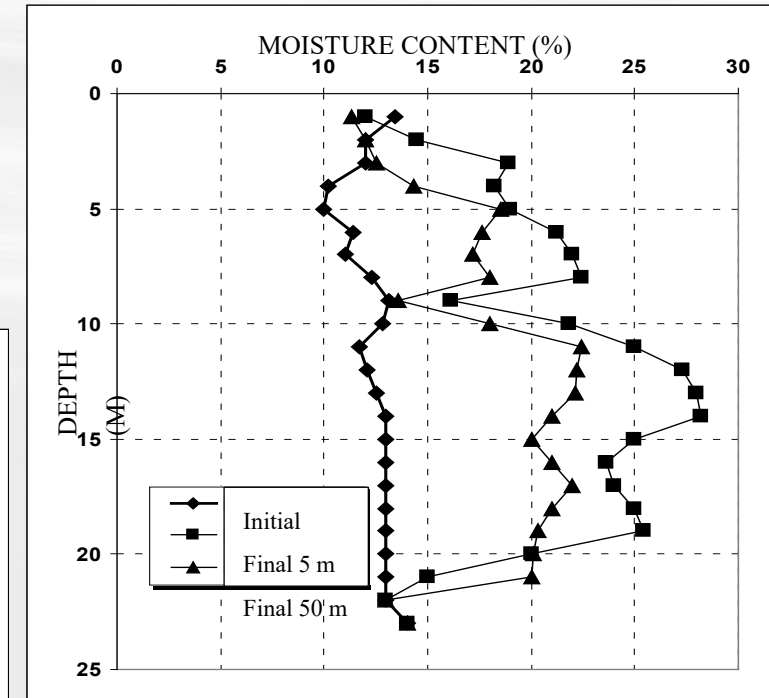
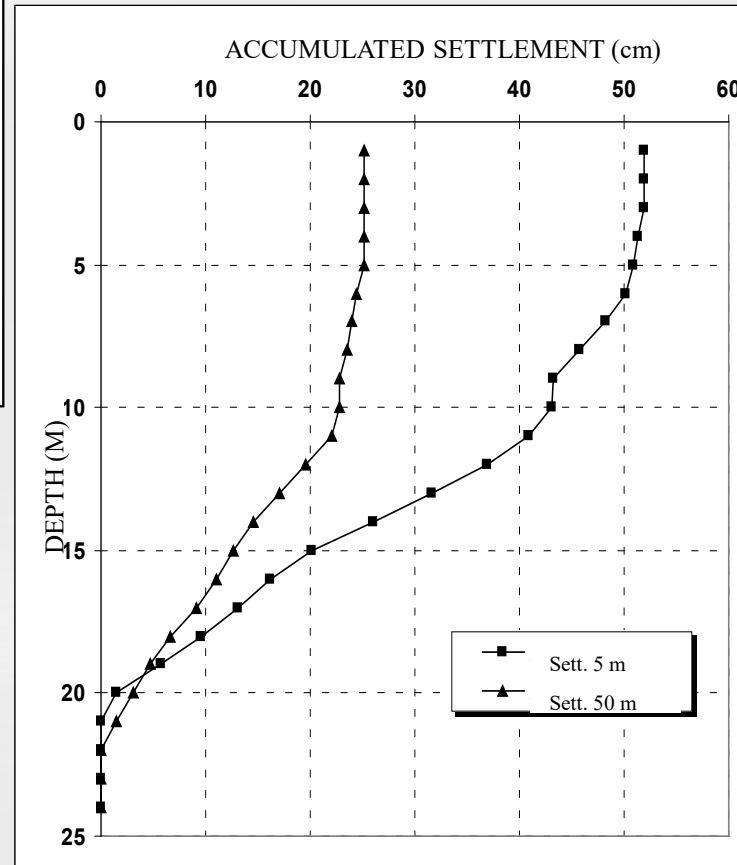
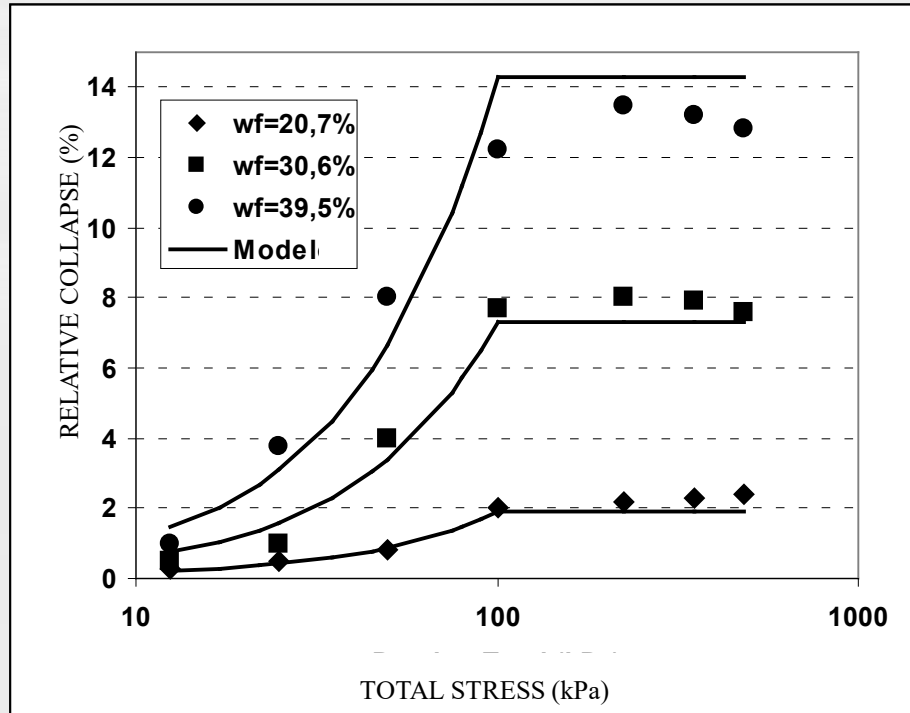
(After Terzariol 2012)

Damage for self-collapse Education Center



Collapsible soils in Argentina

Experiences and case histories



(After Terzariol 2012)

Final Remarks

- **A description of both primary and secondary loessic soils is presented.**
- **Collapsible loessic soils are described, analyzing their regional problems and, in particular, the structures built on them.**
- **The most relevant geomechanical parameters for these soils are provided.**
- **Recommendations are made regarding the most commonly used characterization methods in the field and their results.**
- **An evaluation is carried out of the foundation systems used in Argentina over more than 60 years of experience.**
- **The design methods for these foundations and the expected behaviors with them are presented.**
- **Through two analyses of two local case histories related to foundation and construction problems on collapsible soils, evaluating the construction methodologies employed, the prediction methods commonly used.**
- **Finally, this presentation reflects the experiences of more than 50 years of studies and research carried out to date at the Geotechnical Laboratory of the Faculty of Exact, Physical, and Natural Sciences of the National University of Córdoba, Argentina.**



**UT PORTET NOMEN MEUM
CORAM GENTIBUS**



**Associação Brasileira de Mecânica
dos Solos e Engenharia Geotécnica**

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celebrando o presente e
inspirando o futuro*

21 e 22 de julho de 2025
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